

Designing Long- T_2 Suppression Pulses for Ultrashort Echo Time Imaging

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Ultrashort echo time (UTE) imaging has shown promise as a technique for imaging tissues with T_2 values of a few milliseconds or less. These tissues, such as tendons, menisci, and cortical bone, are normally invisible in conventional magnetic resonance imaging techniques but have signal in UTE imaging. They are difficult to visualize because they are often obscured by tissues with longer T_2 values. In this article, new long- T_2 suppression RF pulses that improve the contrast of short- T_2 species are introduced. These pulses are improvements over previous long- T_2 suppression pulses that suffered from poor off-resonance characteristics or T_1 sensitivity. Short- T_2 tissue contrast can also be improved by suppressing fat in some applications. Dual-band long- T_2 suppression pulses that additionally suppress fat are also introduced. Simulations, along with phantom and in vivo experiments using 2D and 3D UTE imaging, demonstrate the feasibility, improved contrast, and improved sensitivity of these new long- T_2 suppression pulses. The resulting images show predominantly short- T_2 species, while most long- T_2 species are suppressed. Magn Reson Med 56:94–103, 2006. © 2006 Wiley-Liss, Inc.

Key words: ultrashort echo time (UTE) imaging; long- T_2 suppression; T_2 contrast; short- T_2 imaging; RF pulse design

Ultrashort echo time (UTE) imaging is a novel type of magnetic resonance imaging (MRI) that can image tissues with very short T_2 relaxation times. These tissues are normally invisible in all other types of MRI. There are many potential in vivo applications imaging short T_2 species (1), including collagen-rich tissues such as tendons, ligaments, and menisci, as well as calcifications, myelin, periosteum, and cortical bone.

Conventional imaging methods have minimum echo time (TE) requirements and thus can only image species with T_2 values greater than a few milliseconds. UTE imaging, as well as single-point imaging methods such as SPRITE (3) and related multipoint methods (4), begin acquiring data as soon as possible after excitation. In these methods, the TE is limited only by how quickly the MR system can switch from transmit to receive mode, which

depends on electronics switching times as well as coil ring-down time. On present-day clinical MR systems the minimum switching time is about 60–200 μ s, with the shortest TE reported on a clinical 1.5 T system being 8 μ s (5).

Previous studies have explored many UTE imaging applications. These include imaging calcifications, cavernomas, and metastases in the brain (6,7), hemochromatosis and cirrhosis in the liver (8), periosteum (9), lung parenchyma (10,11), tendons and menisci (12), the Achilles' tendon (13), and articular cartilage (14). Recent studies have also investigated using gadolinium for contrast enhancement (15), as well as short- T_2 phosphorus imaging in vivo (16). UTE imaging has also been applied to chemical shift imaging (17) and spectroscopy (14), as well as angiography (18) and temperature mapping in frozen tissue (19). Connective structures such as myelin, capsules, and falx are other potential areas for UTE applications.

Short- T_2 species in UTE imaging often suffer from poor contrast. This is due to surrounding long- T_2 tissues with high signal or overlapping long- T_2 components that obscure the short- T_2 components. In general, the longer T_2 species will have higher signal since they decay slower and thus are easier to image. Long- T_2 suppression is an important technique that improves the contrast and visualization of short- T_2 components.

Multiple methods have been proposed for long- T_2 suppression, all of which can be classified into two groups. The first group consists of methods that combine images acquired with different TEs to create T_2 contrast. The most common technique is to subtract a later echo image, containing signal only from long- T_2 species, from the first echo image (1). Combining multiple different TE images can also create highly T_2 selective images without the need for T_2 fitting (20). Image combination long- T_2 suppression techniques are simple to implement and provide a reference image that is useful for diagnosis. The short- T_2 signal-to-noise ratio (SNR) is decreased by the combination, and artifacts due to off-resonance and T_2^* effects are a problem.

The other group of long- T_2 suppression methods are based on RF pulses. The original method prepares the magnetization with a long rectangular $\pi/2$ pulse followed by a dephaser (21). Short- T_2 species are not excited by the pulse because the decay rate exceeds the excitation rate while long- T_2 species are saturated, creating T_2 contrast. This technique is SNR and contrast efficient, but is very sensitive to off-resonance and inhomogeneous B_1 fields, and does not suppress fat. Another technique, called refocused TELEX, was designed to highlight longer short- T_2 species (> 10 ms) (22). The method uses a long $\pi/2$ pulse routinely interrupted by refocusing pulses to improve the

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Grant sponsor: GE Medical Systems; Grant sponsor: NIH; Grant number: 1R01-EB002524.

Received 15 September 2005; revised 1 March 2006; accepted 15 March 2006

DOI 10.1002/mrm.20926

Published online 24 May 2006 in Wiley InterScience (www.interscience.wiley.com).

off-resonance characteristics of the suppression. Its performance varies with T_1/T_2 .

Inversion recovery (IR) can also be used to selectively null long- T_2 components with a particular T_1 (1). A longer duration inversion pulse will not affect short- T_2 species too much but will have a narrow spectral bandwidth. This technique is T_1 selective.

Fat suppression is also useful in UTE when imaging short- T_2 components that are surrounded by fat, such as tendons, ligaments, menisci, periosteum, and cortical bone. Conventional techniques, such as fat-selective saturation pulses, IR, and Dixon techniques (12), have all been used in UTE imaging. Each of these methods can be applied in addition to long- T_2 suppression.

In this article we describe a new set of RF pulses for long- T_2 suppression. These pulses are more robust to off-resonance than long rectangular pulses without introducing T_1 selectivity or compromising short- T_2 signal levels. We also introduce a new set of dual-band pulses that include long- T_2 suppression at both the water and the fat resonances.

THEORY

Long- T_2 suppression pulses are based on the observation that it is easy to excite long- T_2 species but difficult to excite short- T_2 species. Short- T_2 species aren't affected by low-amplitude, long-duration pulses because their transverse magnetization decays faster than it is excited. As T_2 increases, the excitation rate dominates the transverse relaxation. Thus, long- T_2 species are fully excited and short- T_2 species are relatively unaffected.

When T_2 is much greater than the pulse duration (T_{pulse}) and the excitation rate dominates the transverse relaxation, we can analyze the suppression pulses using standard tools such as the Shinnar-Le Roux (SLR) transform (23).

When T_2 is on the order of or less than T_{pulse} , the transverse relaxation can no longer be neglected. In this case, we do simulations and analysis with the Bloch equation. To simplify the analysis, we assume that the spins are on-resonance, the RF pulse is amplitude modulated, and we neglect T_1 relaxation. The Bloch equation in the rotating frame is reduced to two differential equations:

$$\frac{dM_Y(t, T_2)}{dt} = \frac{-M_Y(t, T_2)}{T_2} + \omega_1(t)M_Z(t, T_2) \quad [1]$$

$$\frac{dM_Z(t, T_2)}{dt} = -\omega_1(t)M_Y(t, T_2), \quad [2]$$

where $\omega_1(t) = \gamma B_1(t)$ is the RF pulse. Using the small-tip approximation ($M_Z(t, T_2) \approx M_0$), a solution for $M_Y(t, T_2)$ can be derived, similar to the proof in (24):

$$M_Y(t, T_2) = M_0 \int_0^t e^{-(t-s)/T_2} \omega_1(s) ds. \quad [3]$$

Equation [3] expresses $M_Y(t, T_2)$ as a convolution of $\omega_1(t)$ and a truncated e^{-t/T_2} , illustrated in Fig. 1. A useful sim-

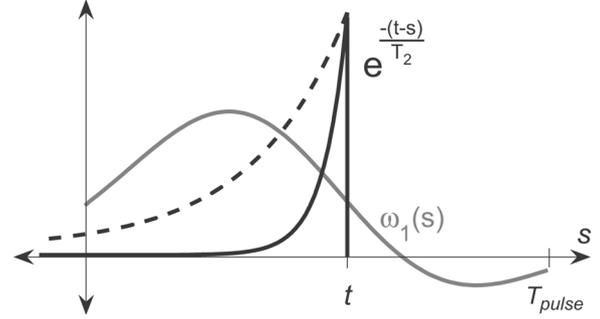


FIG. 1. Graphical illustration of the convolution integral in Eq. [3]. When the RF pulse variations are slower than the T_2 exponential decay, $\omega_1(s)$ is approximately constant and can be removed from the integral, as is done to derive Eq. [6]. This approximation is valid for shorter T_2 values (solid line), but will not hold for longer T_2 values (dashed line).

plification can be made for short enough T_2 values such that the RF pulse is slowly varying relative to the exponential weighting, e^{-t/T_2} . A pulse with a bandwidth, BW, will have oscillations on the time scale of $1/\text{BW}$, while the exponential weighting is mostly decayed within time T_2 . The condition for making this simplification is that $T_2 \ll 1/\text{BW}$, or $T_2 \times \text{BW} \ll 1$. We can then remove $\omega_1(t)$ from the integral in Eq. [3] since it is approximately constant during the exponential weighting, allowing us to derive the following approximate solution for $M_Y(t, T_2)$:

$$M_Y(t, T_2) \approx M_0 \int_0^t e^{-(t-s)/T_2} ds \cdot \omega_1(t) \quad [4]$$

$$= M_0 T_2 (1 - e^{-t/T_2}) \cdot \omega_1(t) \quad [5]$$

$$\approx M_0 T_2 \cdot \omega_1(t). \quad [6]$$

This result indicates how short- T_2 species decay faster than excited and also that the transverse magnetization is approximately proportional to T_2 when $T_2 \times \text{BW} \ll 1$.

Finally, we revisit the longitudinal magnetization and refine our model by assuming that it is not constant. $M_Z(t, T_2)$ is then solved by substituting the result from Eq. [6] into Eq. [2]. After integrating the differential equation to the end of the pulse, $t = T_{\text{pulse}}$, with the initial condition that $M_Z(0, T_2) = M_0$, the resulting longitudinal magnetization is

$$M_Z(T_{\text{pulse}}, T_2) \approx M_0 (1 - T_2 \int_{-\infty}^{\infty} \omega_1(t)^2 dt), \quad [7]$$

with $\omega_1(t) = 0$ for $t < 0$ and $t > T_{\text{pulse}}$. The change in M_Z is proportional to T_2 multiplied by the RF power, irrespective of the pulse shape. We will use this flexibility in designing the suppression pulses.

We can gain more insight by applying Rayleigh's Theorem to Eq. [7]:

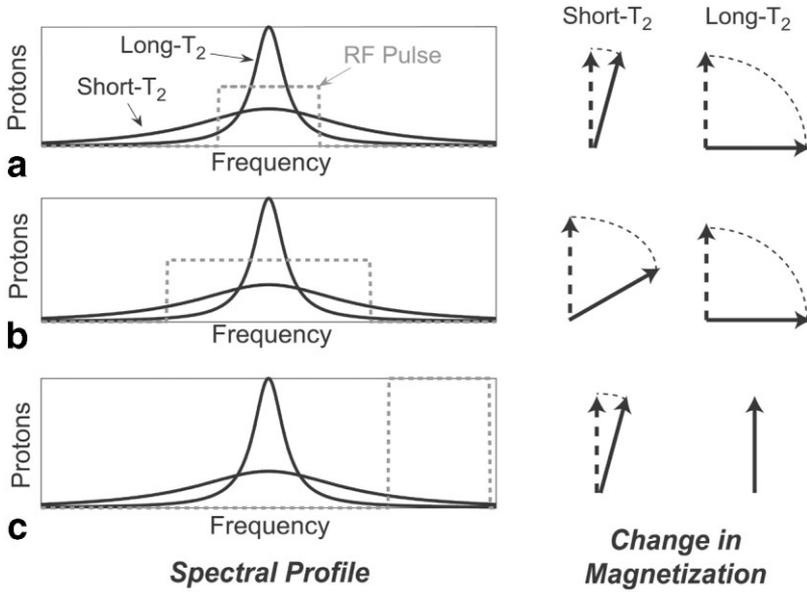


FIG. 2. Spectral linewidth (proportional to T_2) and RF pulse bandwidth determine excitation (Eq. [8]). (a) Narrow bandwidth (dashed line) RF pulse that overlaps with the majority of the long- T_2 spectrum but only a small fraction of the short- T_2 spectrum. The long- T_2 species is excited more by the pulse than the short- T_2 species. (b) Wide bandwidth (dashed line) RF pulse that overlaps with both long- and short- T_2 spectra, thus exciting both. (c) Magnetization transfer (MT) pulses applied off-resonance primarily excite short- T_2 species.

$$M_z(T_{\text{pulse}}, T_2) \approx M_0(1 - T_2 \int_{-\infty}^{\infty} |\Omega_1(f)|^2 df), \quad [8]$$

where $\Omega_1(f)$ is the Fourier transform, or frequency spectrum, of the RF pulse. This shows a trade-off between total RF spectral power and short- T_2 attenuation.

Equation [8] can also be understood in terms of spectral linewidths. T_2 is inversely proportional to the linewidth, meaning that short- T_2 species have broad linewidths and long- T_2 species have narrow linewidths. The overlap between the spectrum of the RF pulse and the tissue spectrum determines the excitation, shown in Fig. 2. The narrow spectrum of a long- T_2 species is more easily covered by the RF spectrum and thus is easily excited. (This result is also derived in (22).) The broad short- T_2 species spectrum requires a wide bandwidth RF pulse to be excited. A narrow bandwidth RF pulse will fully excite the longer T_2 species but only partially excite the shorter T_2 species, making it an effective long- T_2 suppression pulse.

Main magnetic field inhomogeneity causes resonance shifts in protons. T_2^* includes the effects of these shifts when summed over a tissue or voxel. For short- T_2 species, these shifts are generally small relative to the linewidth, so the field inhomogeneity does not affect the preceding analysis. Resonance shifts on the order of the pulse bandwidth will compromise the suppression of long- T_2 species, as shown in the Results.

METHODS

Pulse Design

Equation [8] shows that short- T_2 attenuation is approximately linear with pulse bandwidth. This means that long- T_2 suppression pulses will be limited in bandwidth, but carefully choosing how this bandwidth is used will reduce off-resonance sensitivity. Desirable spectral profile characteristics are flat suppression bands, short transition widths, and minimal excitation out of the suppression

band. The flat suppression band will suppress long- T_2 species at a wide range of resonances, while a short transition width and minimal out-of-band excitation will reduce undesired short- T_2 attenuation. The SLR pulse design algorithm is well suited to long- T_2 suppression pulse design because it can produce the desired spectral profile characteristics and the resulting pulses are minimum power for a chosen profile (23).

Suppression, or saturation, pulses do not require a linear phase and will benefit from having nonlinear phase, which allows for shorter transition bands and also introduces phase dispersion into the saturated magnetization. We achieve nonlinear phase by first designing a linear phase filter using Parks–McClellan digital filter design algorithms (25). The filter roots are manipulated to produce a maximum-phase pulse, as described in (23). The resulting maximum-phase filter is converted to an RF pulse using the SLR transform. Using other nonlinear phase profiles is not necessary because they will not improve the spectral or T_2 profile and peak power is not a concern for these low-amplitude pulses.

Single-Band Pulses

Single-band long- T_2 suppression pulses have one spectral saturation band to suppress long- T_2 species on the water proton resonance. These are maximum-phase saturation pulses created using the SLR pulse design algorithm with Parks–McClellan filter design, as described in (23).

The primary design parameter is the time \times bandwidth product (TBW), which is proportional to the spectral profile sharpness. The bandwidth in the TBW product is the full-width, half-maximum (FWHM) bandwidth of the filter, which corresponds to the $M_z = 0.75 M_0$ bandwidth of a saturation pulse and is also proportional to the short- T_2 attenuation. The FWHM bandwidth (BW_{FWHM}) is wider than the range of off-resonances that will be adequately suppressed. A few rules of thumb for a given BW_{FWHM} are that T_2 (ms) = $2000/BW_{\text{FWHM}}$ (Hz) will be reduced to 10%

of its initial magnetization, while $T_2 = 1000/BW_{\text{FWHM}}$ will be at 20% and $T_2 = 300/BW_{\text{FWHM}}$ at 50% of their initial magnetizations.

The TBW product is a trade-off between the pulse duration and profile sharpness since the FWHM bandwidth is generally constrained by the desired short- T_2 response and/or expected off-resonances. Rectangular suppression pulses are $TBW \approx 1$, resulting in a poor profile but a short pulse length. We have generally used pulses with a TBW between 2 and 3, as they have a reasonably flat spectral profile, which is a significant improvement on the rectangular pulse profile. Higher TBW pulses have slightly sharper profiles but they must be longer, during which T_1 relaxation effects may compromise the suppression. A single-band pulse with TBW of N must be N times as long as a rectangular pulse to have the same T_2 response. We have primarily used single-band pulses between 10 and 40 ms in length.

The other design parameters are the passband and stop-band ripples and the filter order. Ripple values of 1% are sufficient for these pulses. We used a filter order of 250, but this is more than necessary and orders as low as 20 would probably be sufficient. A pulse designed with a given TBW can be stretched in time to change the T_2 response and FWHM bandwidth.

Dual-Band Pulses

Dual-band long- T_2 suppression pulses have two spectral saturation bands at the fat and water resonances to suppress long- T_2 species at both resonances. They are created by first designing a dual-band filter using the complex Parks–McClellan algorithm (26). The resulting equiripple linear phase filter is converted into a maximum-phase filter, which is transformed to an RF pulse using the SLR transform.

The design parameters are the pulse duration, suppression bandwidths, fat band frequency offset, filter order, and desired ripple values. The suppression bandwidths are not FWHM bandwidths and instead correspond to the actual range of off-resonances suppressed. Typically we use suppression bandwidths of 60 to 100 Hz on-resonance and 80 to 150 Hz at the fat resonance, which is centered around -220 to -260 Hz. A filter order of 100 to 200 and ripple values of 0.5% are adequate. The pulses require 20 to 30 ms, and longer durations will result in narrower transition widths. The transition width is calculated as $\Delta f = D_{\text{inf,m}}(\delta_1, \delta_2)/T_p$, where T_p is the pulse length, δ_1 and δ_2 are the suppression band and out-of-band ripples values, and $D_{\text{inf,m}}(\delta_1, \delta_2)$ is defined in (23). Transition widths between 30 and 60 Hz are typical. Narrower transition regions will result in slightly less short- T_2 attenuation.

Sample Pulses

Figure 3 shows three long- T_2 suppression pulses used in both phantom and in vivo experiments. The 16-ms rectangular and 40-ms $TBW = 2.4$ single-band pulse have approximately identical T_2 profiles, with FWHM bandwidths of 62.5 and 60 Hz, respectively. The 25-ms dual-band pulse was designed with suppression bandwidths of 80 Hz

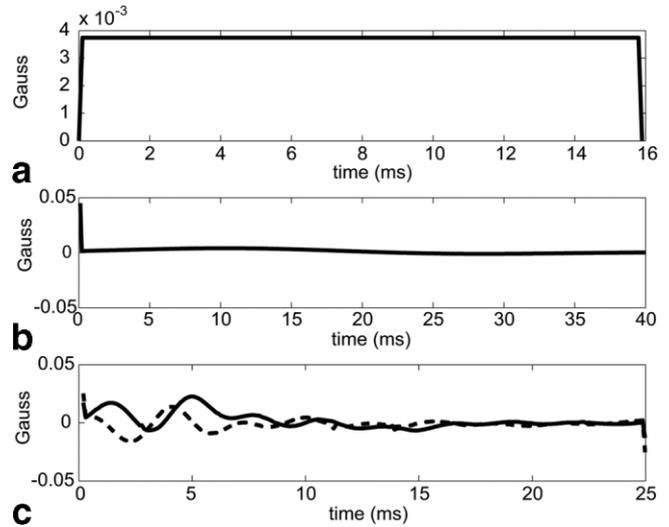


FIG. 3. Long- T_2 suppression pulses. (a) 16-ms rectangular suppression pulse. (b) 40-ms $TBW = 2.4$ single-band suppression pulse. (c) 25-ms dual-band suppression pulse with 80-Hz water suppression bandwidth and 140-Hz suppression centered at -255 Hz for fat suppression—both real (solid line) and imaginary (dashed line) components are shown.

on-resonance and 140 Hz centered at -255 Hz off-resonance for fat suppression.

The long- T_2 suppression pulses were designed in Matlab 7.0 (The Mathworks, Natick, MA, USA). The design functions, accompanying documentation, and sample pulses are available for general use at <http://www-mrsrl.stanford.edu/~peder/longt2supp>.

Simulations

To initially validate the performance of the RF pulses, we simulated their off-resonance and T_2 profiles. We used a Bloch equation simulation that calculates the precession and decay matrices using the RF waveforms for each of a set of resonant frequencies. This Bloch simulation was coded in Matlab and is available at <http://www-mrsrl.stanford.edu/~brian/blochsim>. Off-resonance simulations used $T_2 = 100$ ms, $T_1 = 1$ s, and frequencies relative to water protons at 1.5 T.

Experiments

A GE Excite 1.5 T scanner with gradients capable of 40 mT/m amplitude and 150 T/m/s slew rate (GE Healthcare, Milwaukee, WI, USA) was used for all experiments. The minimum TE of our configuration was 80 μ s, limited by the coil ring-down time and hardware switching times.

Both 2D and 3D UTE sequences were used. A 2D sequence is shown in Fig. 4. The long- T_2 suppression pulses and an accompanying dephaser gradient were applied as contrast preparation before the imaging sequences. A half-pulse excitation was used in the 2D sequence, where two acquisitions with alternating slice select gradients are summed to obtain the full-pulse slice profile (10,11). A slice prephasing gradient was also used to eliminate spa-

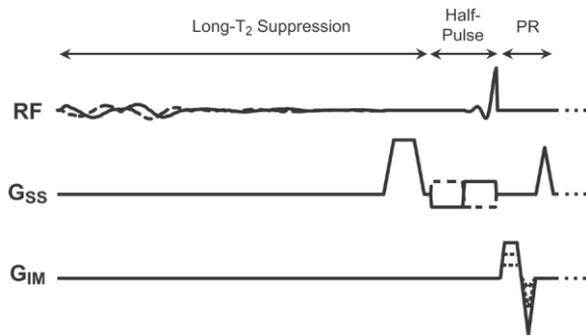


FIG. 4. 2D UTE imaging sequence. The long- T_2 suppression pulse along with a dephasing gradient is played out before the half-pulse excitation. The slice-select gradient is inverted (dashed-line) between acquisitions to turn the half-pulse into a full pulse. A slice prephasing gradient is also included to allow for acquisition of off-isocenter slices. A projection reconstruction (PR) readout is used, and the above sequence is repeated every TR. In a 3D acquisition, the half-pulse and slice-select gradient are replaced by a hard pulse, and a twisted PR trajectory (27) is used.

tially dependent phase terms that arise when acquiring off-isocenter slices. Without this prephaser, these phase terms will distort the slice profile when the two acquisitions are summed.

The 3D sequence does not require slice-selective excitation and instead uses a hard pulse. This eliminates several problems associated with half-pulses, including sensitivity to timing errors, eddy current artifacts (19), compromised slice profiles for short- T_2 s, and large excitation tails that make multislice scanning difficult. The 3D acquisition requires a longer scan time and shimming over a large volume.

A projection reconstruction (PR) radial readout with a 125- or 250-kHz sampling bandwidth was used in the 2D imaging to acquire the quickly decaying short- T_2 data as rapidly as possible. We limited the acquisition time to 1 ms. In 3D imaging we used a twisted 3D PR trajectory that is significantly faster than 3D PR while maintaining the field of view (FOV) and resolution (27). The repetition time (TR), number of readouts, and samples per readout varied across experiments.

T_2 phantoms were created by doping distilled water with manganese chloride (MnCl_2), resulting in T_2/T_1 values of 0.3/2, 0.6/4, 1.2/7, 2.4/15, 4/30, 4.8/35, 6/40, 10/70, 20/100, 50/250, and 100/460 ms. They were imaged using a 2D UTE sequence with $\text{TE} = 80 \mu\text{s}$, flip angle = 60° , 5-mm slice thickness, 1-mm in-plane resolution, and $\text{TR} = 200 \text{ ms}$, 1 s, or 2 s, chosen such that $\text{TR} \geq 4 \times T_1$. A transmit/receive head coil was used.

Off-resonance data was acquired with the $T_2/T_1 = 100/460 \text{ ms}$ phantom by applying linear gradients to induce resonance shifts, which were quantified using a field map. Many of the phantoms experienced nonnegligible T_1 recovery because their T_1 was on the order or less than the suppression pulse durations. The T_1 recovery was compensated for in postprocessing using the pulse durations and the delay between suppression and excitation.

In vivo experiments were performed on healthy volunteers. All subjects gave informed consent in accordance

with Stanford University policy after they were screened for possible MRI risk factors. Brain images were acquired with a 2D UTE sequence with $\text{TE} = 80 \mu\text{s}$, $\text{TR} = 500 \text{ ms}$, flip angle = 60° , 4:15 per image, 5-mm slice thickness, and 1-mm in-plane resolution. Later TE s of 2.3, 4.7, and 9.4 ms were also acquired to create field maps and subtraction images. A transmit/receive head coil was used. 3D UTE imaging was done on the ankle and knee with 0.6-mm isotropic resolution, $\text{TR} = 100 \text{ ms}$, $\text{TE} = 80 \mu\text{s}$, and a 7-cm FOV. A total of 12000 spokes of a twisted 3D PR trajectory were acquired in 20 min of total scan time. Ankle imaging was done with a 3-inch surface coil. Knee images were acquired using a transmit/receive extremity coil. Shimming for 3D acquisitions was done manually using a quickly acquired field map.

The bandwidth of the long- T_2 suppression pulses was chosen based on the desired application. In the brain we found that $\pm 15 \text{ Hz}$ of suppression bandwidth was necessary for a single slice; thus, we chose a 40-ms $\text{TBW} = 2.4$ single-band suppression pulse, shown in Fig. 3b, and compared it to a 16-ms rectangular pulse, shown in Fig. 3a. In the ankle and knee we needed at least $\pm 30 \text{ Hz}$ suppression bandwidth for the volume, so we used a 25-ms dual-band pulse with $\pm 40 \text{ Hz}$ suppression bandwidth at water and $\pm 70 \text{ Hz}$ centered around -255 Hz for fat suppression (Fig. 3c).

RESULTS

Simulations

Figure 5 compares the relationship derived in Eq. [7] with simulations over a range of short- T_2 values for three different pulse shapes: a 16-ms rectangular pulse, a 32-ms $\text{TBW} = 2$ pulse, and a 64-ms $\text{TBW} = 4$ pulse, each of which have a FWHM bandwidth = 62.5 Hz. There is reasonable agreement for each of these pulses in the shown time scale, which has a maximum $T_2 \times \text{BW} \approx 0.03 \ll 1$,

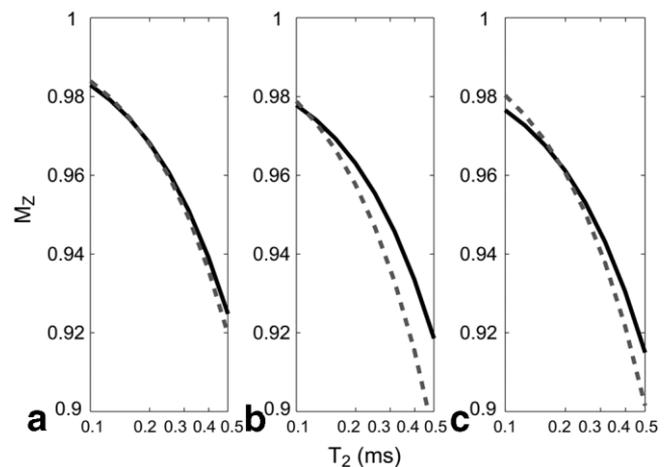


FIG. 5. T_2 profile from Bloch equation simulations (solid lines) and the approximation derived in Eq. [7] (dashed lines). (a) 16-ms rectangular pulse. (b) 32-ms $\text{TBW} = 2$ pulse. (c) 64-ms $\text{TBW} = 4$ pulse. The approximation and simulation agree reasonably well for each of the three pulse shapes over the T_2 ranges shown, but the approximation degrades as T_2 increases.

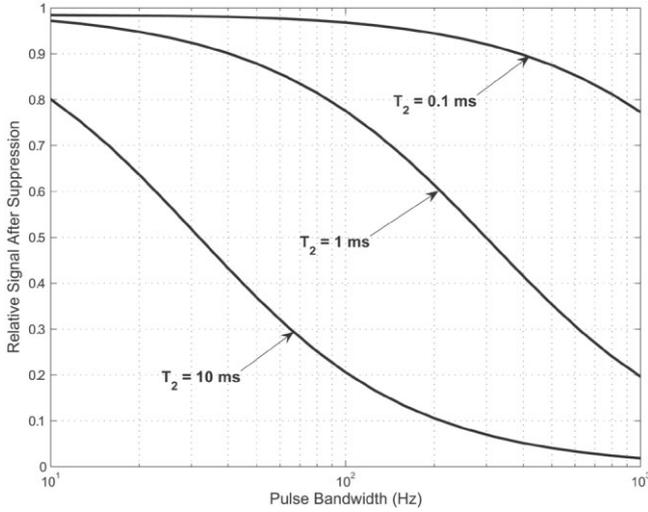


FIG. 6. Simulation results for the longitudinal magnetization remaining after single-band suppression pulses of different bandwidths for various T_2 values. As the pulse bandwidth increases, the signal remaining after suppression decreases, as predicted by Eq. [8]. As T_2 increases, the signal also decreases.

satisfying the approximation used to derive Eq. [7]. The agreement degrades as T_2 increases because this condition is violated.

The Bloch equation simulation results in Fig. 6 confirm the relation between pulse bandwidth and longitudinal magnetization after suppression derived in Eq. [8]. As the pulse bandwidth increases, the remaining signal decreases, as expected, with varying rates depending on T_2 . Also as expected, the remaining signal decreases as T_2 increases. Note that the different T_2 curves are simply shifted versions of each other, meaning that the remaining magnetization will be approximately constant for a constant $T_2 \times \text{BW}$ product. This product shows up in Eq. [8] as $T_2 \int_{-\infty}^{\infty} |\Omega_1(f)|^2 df$.

Figure 7 compares the 16-ms rectangular and 40-ms TBW = 2.4 single-band suppression pulses shown in Figs. 3a and b. The T_2 profiles are nearly identical, as we expect because the pulses have similar FWHM bandwidths of 62.5 and 60 Hz, respectively. They both retain 90% of the initial magnetization for $T_2 = 600 \mu\text{s}$, 50% for $T_2 = 5 \text{ ms}$, and 10% for $T_2 \approx 30 \text{ ms}$. The single-band pulse has an improved off-resonance profile, with a factor of 20 suppression bandwidth of 30 Hz, compared to 10 Hz for the rectangular pulse. This is approximately a factor of 3 improvement without compromising the short- T_2 attenuation. The rectangular pulse wastes power in its wide transition region and passband ripples, seen around $\pm 90 \text{ Hz}$ in Fig. 2b.

When a second band for long- T_2 fat suppression is added to the pulses, we expect to see an increase in short- T_2 attenuation. Figure 8 compares the 25-ms dual-band pulse from Fig. 3c (solid line) to a 25-ms dual-band pulse with a narrower fat suppression band (dashed line) and a 25-ms TBW = 3.4 single-band pulse (dotted line). The water-resonance T_2 profile in Fig. 8a shows this increase in short- T_2 attenuation in the dual-band pulses. All

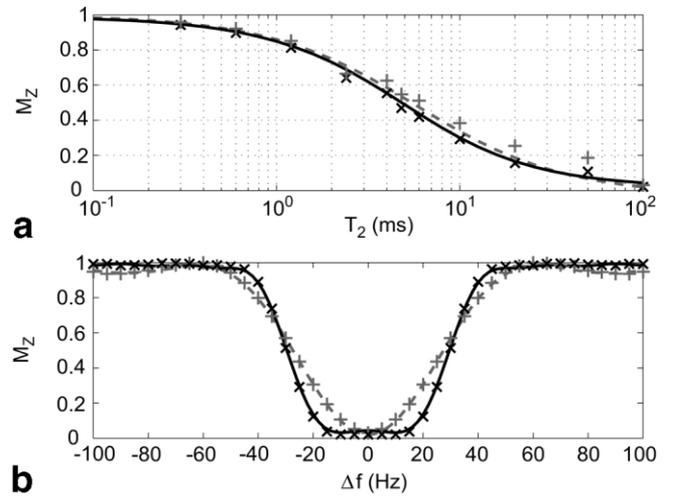


FIG. 7. Simulation and phantom experiment results comparing the 16-ms rectangular (dashed line, +) and 40-ms TBW = 2.4 single-band (solid line, \times) suppression pulses shown in Figs. 3a and b. (a) On-resonance T_2 profiles. (b) Off-resonance profiles for $T_2 = 100 \text{ ms}$. The data show that the pulses have nearly identical T_2 profiles, but the single-band pulse off-resonance performance is superior. The phantom data agrees well with the simulations, with the exception of less than expected suppression for $T_2 > 10 \text{ ms}$ phantoms with the rectangular pulse.

three pulses have a factor of 20 suppression bandwidth of 80 Hz on-resonance, and the single-band pulse has a FWHM bandwidth of 136 Hz. Widening the fat suppression band has only a small effect on short- T_2 species while

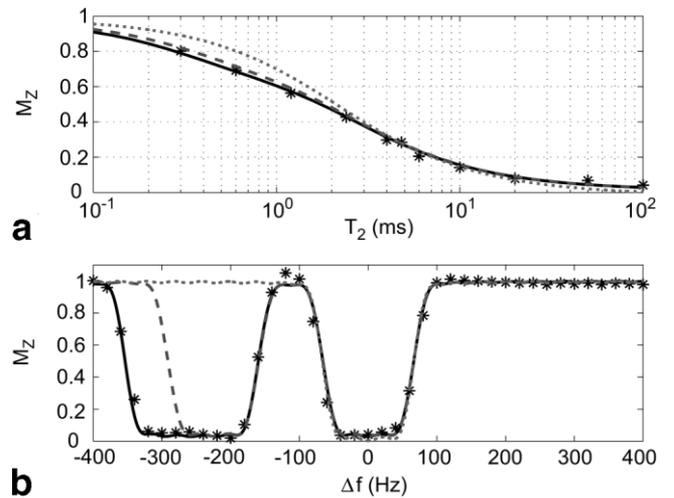


FIG. 8. Effect of adding a fat suppression bands. (a) On-resonance T_2 profile. (b) Off-resonance profile for $T_2 = 100 \text{ ms}$. The dual-band pulse used in vivo, shown in Fig. 3c, is represented by the solid line (simulations) and $*$ (experiments). Using a pulse with a narrower fat suppression band (dashed line, simulated data) has only a small effect on the short- T_2 signal. When compared to a 25-ms TBW = 3.4 single-band pulse (dotted line, simulated data), which has the same water suppression bandwidth, the dual-band pulses have approximately 10% additional signal loss for $T_2 < 1 \text{ ms}$.

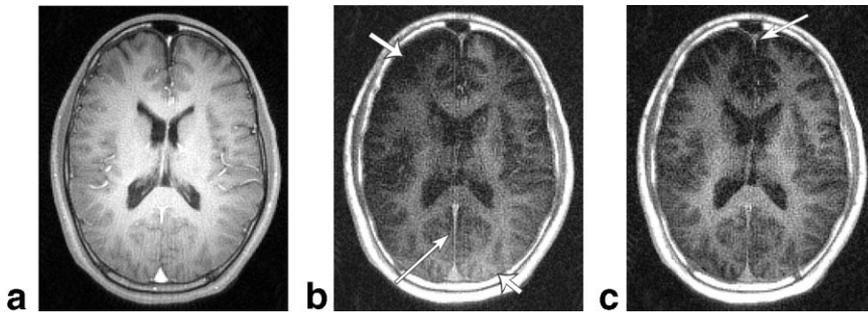


FIG. 9. UTE Brain images with and without long- T_2 suppression. (a) Unsuppressed image. (b) 16-ms rectangular suppression pulse. (c) 40-ms TBW = 2.4 single-band suppression pulse. With the suppression pulses, short- T_2 components in the white matter, likely from myelin, are visible, as is the falx cerebri (long, thin arrows). The rectangular pulse suppression in (b) is variable across the slice (short, fat arrows), while the single-band pulse produces consistent suppression in (c).

reducing the chance of fat suppression failure due to off-resonance.

Experiments

Data from T_2 phantom experiments is plotted with the simulated T_2 and off-resonance profiles in Figs. 7 and 8. The off-resonance data in Fig. 2b agrees excellently with the simulated results for both pulses. There is also excellent agreement in Fig. 2a for the 40-ms TBW = 2.4 suppression pulse (\times). The 16-ms rectangular pulse data (+) shows some disagreement, especially at $T_2 = 20$ and 50 ms. This could be the result of averaging over small resonance shift ranges, which would increase the signal because of the narrow suppression bandwidth. The phantom data in Fig. 8 were acquired using the 25-ms dual-band pulse from Fig. 3c. Both the on-resonance T_2 data and off-resonance data agree well with the simulated results.

Figures 9 and 10 show brain UTE images with and without long- T_2 suppression for two different volunteers. The use of long- T_2 suppression pulses reveals a white matter short- T_2 component that is completely obscured without suppression. We believe that this component is associated with myelin, as has previously been suggested by its absence in patients with multiple sclerosis (1,7).

Short- T_2 components in the falx cerebri (long, thin arrows in Fig. 9) also have significantly improved visualization with suppression. The rectangular and single-band long- T_2 suppression pulses have identical T_2 profiles, and thus they produce similar contrast.

The rectangular pulse suppression (Figs. 9b and 10d) produces varying contrast across the image and poorer delineation of the white matter short- T_2 component than the single-band pulse suppression (Figs. 9c and 10e). There are areas of signal dropout and failed suppression, indicated by the short, fat arrows. These failures are likely due to the narrow bandwidth of the rectangular suppression pulse, similar to the suppression failures observed in longer T_2 phantoms in Fig. 7a. The field map in Fig. 10c corroborates this claim, as the suppression failures with the rectangular suppression pulse in Fig. 10d correlate with the largest off-resonance frequencies. As the off-resonance approaches ± 20 Hz, the suppression fails, as we would expect from the results in Fig. 7b.

Long- T_2 suppression with the single-band pulse is more consistent due to its improved off-resonance profile, resulting in clear and consistent delineation of the white matter short- T_2 component. Subtracting a TE = 9.7 ms image from the TE = 80 μ s image (Fig. 10a) produces the image shown in Fig. 10c. This result shows the falx cerebri

FIG. 10. Brain images with various long- T_2 suppression techniques. (a) Unsuppressed image. (b) B_0 field map. (c) Subtraction suppression using a TE = 9.7 ms image. (d) 16-ms rectangular suppression pulse. (e) 40-ms TBW = 2.4 single-band suppression pulse. The failure with the rectangular suppression pulse (arrows in (d)) roughly corresponds to off-resonance frequency, shown in (b), especially as this approaches ± 20 Hz. The subtraction image (c) is also inconsistent, while the single-band suppression pulse (e) produces the most consistent suppression.

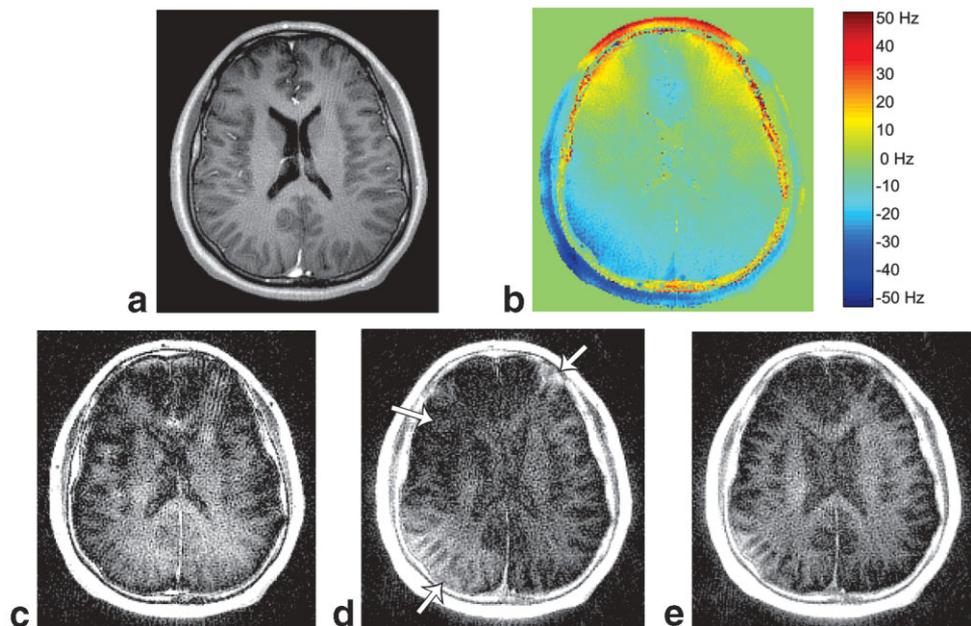
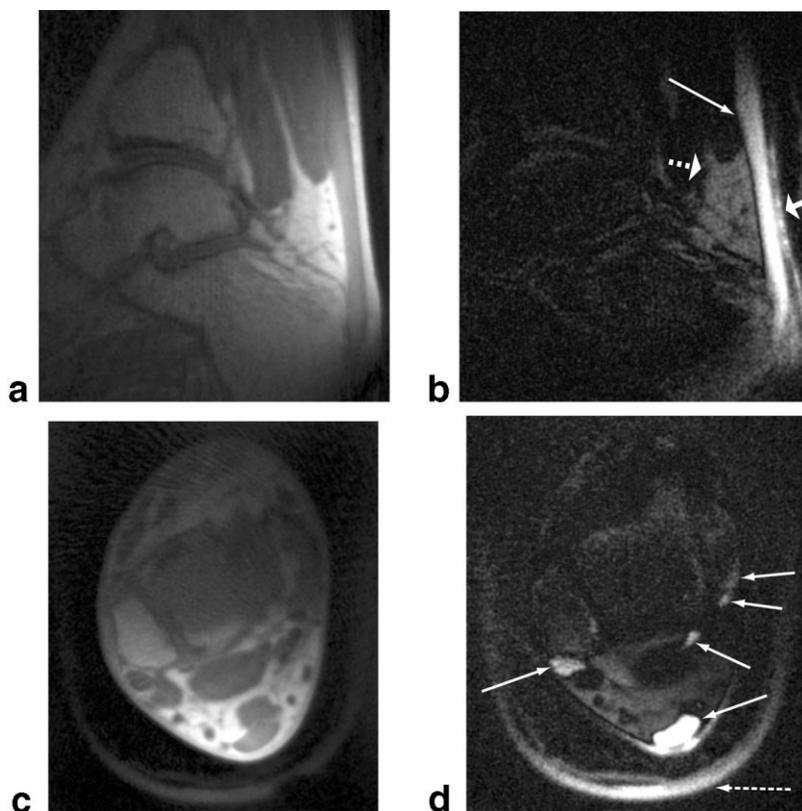


FIG. 11. 3D UTE ankle images. Sagittal slice (a) without suppression and (b) with a dual-band long- T_2 suppression pulse. Axial slice (c) without suppression and (d) with suppression. The suppression significantly improves the contrast of the tendons, such as the Achilles' tendon in (b) and (d), and the peroneal, flexor hallucis longus, flexor digitorum longus, and tibialis posterior tendons in (d) (long, thin arrows). The plastic boot holding the ankle can also be seen (long, dashed arrow in (d)). Unsuppressed signal in the fat pad anterior to the Achilles' tendon (short, dashed arrow in (b)) may be due to short- T_2 components in the fat or suppression failure. Posterior to the Achilles' tendon there is also either failed suppression and/or signal from collagen in the skin (short, solid arrow in (b)).



but the visualization of the short- T_2 component in the white matter is poor and inconsistent. Previous brain UTE studies have produced more promising image subtraction results, sometimes in conjunction with IR to null the long- T_2 white matter component for improved contrast (1,7). In all of our experiments, the short- T_2 component delineation is clearer when using a single-band suppression pulse, as opposed to subtraction or a rectangular suppression pulse.

Ankle images acquired with and without a dual-band long- T_2 suppression pulse are shown in Fig. 11. The muscle and fat are well suppressed by the dual-band pulse. The Achilles' tendon, measured to have two short- T_2^* components of 0.53 (88%) and 4.80 ms (12%) posteriorly and 0.60 (70%) and 4.20 ms (30%) anteriorly (13), is extremely visible in Fig. 11b (long, thin arrow). It is visible again in Fig. 11d, as are the peroneal, flexor hallucis longus, flexor digitorum longus, and tibialis posterior tendons (long, thin arrows). Additionally, the plastic in the boot bracing the foot can be seen (long, dashed arrow). There is still some signal remaining in the fat pad anterior to the Achilles' tendon (short, dashed arrow in Fig. 11b), which may be due to failed suppression or short- T_2 components in the fat. There is also strong signal posterior to the Achilles' tendon (short, solid arrow in Fig. 11b), which may be from the collagen in the skin or an off-resonance artifact due to susceptibility differences at the air-tissue interface.

The knee images in Fig. 12 show similar improvements in short- T_2 contrast when a dual-band suppression pulse was applied. The patellar tendon and menisci have significantly improved contrast in Figs. 12b, c, and

d (long, thin arrows). Figure 12d shows the iliotibial band and anterior cruciate ligament (dashed arrows), as well as thickened tibial cortex in the weight-bearing region of the knee (double arrow). Resonance shifts caused the suppression to fail in the fat near the patella (a common location of fat-saturation failure) and posterior to the femoral condyles, seen in Fig. 12b (short, fat arrows). Note that the cartilage, generally thought of as a short- T_2 , is suppressed since it has a T_2 around 25–45 ms (28).

DISCUSSION

The dual-band and single-band long- T_2 suppression pulses generate excellent short- T_2 contrast and reveal short- T_2 components obscured by long- T_2 components. They show promise for use in UTE imaging.

The primary difficulty in applying the single and dual-band long- T_2 suppression pulses is due to the trade-off between short- T_2 signal and bandwidth. Since we wanted to maximize both, we often pushed the limits of the shimming system to increase short- T_2 signal, making off-resonance artifacts more likely. Choosing the appropriate pulse bandwidth is difficult and will differ by imaging application. For example, extremity imaging has more susceptibility artifacts at tissue-air interfaces and will require a larger bandwidth, whereas brain tissue is more uniform and can tolerate a narrower bandwidth.

The range of short- T_2 values for which we expect this technique to perform well for is limited due to this trade-off. With our technique, tissues with T_2 values less

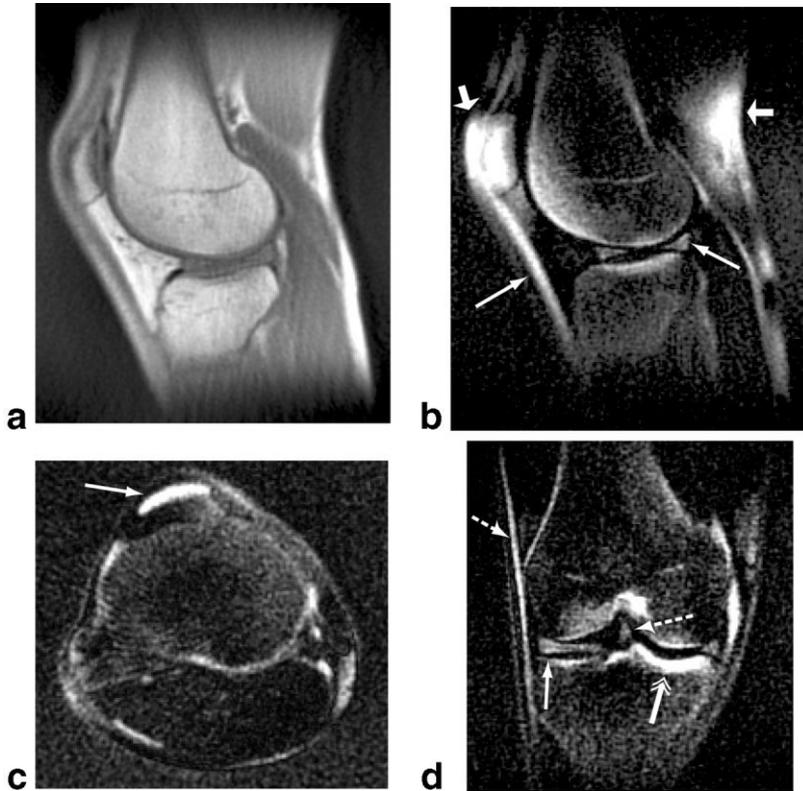


FIG. 12. 3D UTE knee images. Sagittal slice (a) without suppression and (b) a dual-band long- T_2 suppression pulse. (c) Axial and (d) coronal slices with suppression. The suppression enhances the contrast of the short- T_2 structures. The menisci and patellar tendon are particularly visible in (b), (c), and (d) (long, thin arrows). (d) also shows the iliotibial band and the anterior cruciate ligament (dashed arrows), as well as thickened tibial cortex in the weight-bearing region of the knee (double arrow). There is some fat suppression failure around the patella (short, fat arrows in (b)).

than a few milliseconds will have relatively good signal. We expect to be able to image tissues with higher T_2 values, up to about 10 ms, but the suppression pulses may attenuate the signal. Tissues with T_2 values longer than about 10 ms will be difficult to image unless the main magnetic field is very uniform across the area of interest.

For the reasons just described, a good shim significantly improves image quality. In our 3D imaging experiments we acquired a 3D field map and then manually adjusted the shim coils. This was especially useful for 3D volumes in the foot and knee, where there is significant resonance frequency variation. Only a couple minutes were required to complete this process.

The pulses presented will suppress flowing fluid provided it has a long- T_2 and is within the off-resonance tolerance of the pulses. This is shown by the lack of blood signal in Figs. 11 and 12.

The single- and dual-band suppression pulses are not robust to variations in B_1 . We investigated using adiabatic or composite pulses. An adiabatic half-passage can be used for saturation, but has very poor off-resonance characteristics. Using a BIR-4 pulse solves the off-resonance problem (29), but destroys all short- T_2 magnetization. Composite pulses require multiple excitations that also destroy most of the short- T_2 signal (30).

There are alternatives to using a dual-band suppression pulse for fat suppression. One example would be using frequency-selective IR to null fat in conjunction with a single-band suppression pulse. This might improve short- T_2 signal slightly, but the imaging sequence must include the inversion time. Image subtraction could also

be used to suppress fat, but the SNR would be degraded by a factor of $1/\sqrt{2}$ because the second echo time image only adds noise to the short- T_2 components.

Long- T_2 suppression pulses offer significant contrast improvements in 3D UTE imaging, where signal from the whole volume in the center of k -space can inhibit the dynamic range. This makes it difficult to get contrast from short- T_2 species because the long- T_2 species dominate most of the dynamic range. The suppression also sparsifies the signal, which allows for higher undersampling ratios because there will be fewer tissues with signal to cause artifacts. This allows for scan time reductions, which are especially beneficial in 3D radial imaging.

In some applications, long- T_2 suppression may not be required but short- T_2 contrast enhancement would be beneficial. To achieve this, a suppression pulse could be applied, but with a less than $\pi/2$ flip angle, creating a contrast preparation pulse. The long- T_2 species would be partially suppressed, improving the short- T_2 contrast. Less short- T_2 signal would be lost with a contrast pulse compared to a suppression pulse.

CONCLUSION

We have introduced a set of new single-band long- T_2 suppression pulses designed using the SLR pulse design algorithm. We have derived an inherent trade-off between short- T_2 signal and bandwidth, meaning that long- T_2 suppression pulses should be narrow bandwidth and will be susceptible to off-resonance artifacts.

Our single-band pulses are more robust to off-resonance than rectangular pulses while maintaining the same T_2 contrast. They do not introduce any significant T_1 selectivity. We have also introduced dual-band long- T_2 suppression pulses that additionally suppress fat with minimal damage to short- T_2 species. The suppression pulse simulation results were confirmed by T_2 phantom experiments. Single-band pulses used in brain UTE imaging showed improvement over rectangular pulses and subtraction. Dual-band pulses were applied in ankle and knee UTE imaging, creating excellent contrast for tendons, menisci, and other short- T_2 tissues. These are just a few of the potential applications for these suppression pulses in short- T_2 imaging.

ACKNOWLEDGMENTS

We thank Brian Hargreaves for his MATLAB software and Chuck Cunningham for assistance with the MnCl_2 phantoms.

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